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European Patent Office
Office européen des brevets



Publication number:

0 418 781 A2

EUROPEAN PATENT APPLICATION

Application number: 90117858.2

Int. Cl.⁵: **H04B 7/00**

Date of filing: 17.09.90

Priority: 18.09.89 JP 242892/89
16.05.90 JP 126162/90
17.05.90 JP 128059/90
17.05.90 JP 128059/90

Date of publication of application:
27.03.91 Bulletin 91/13

Designated Contracting States:
DE FR GB IT

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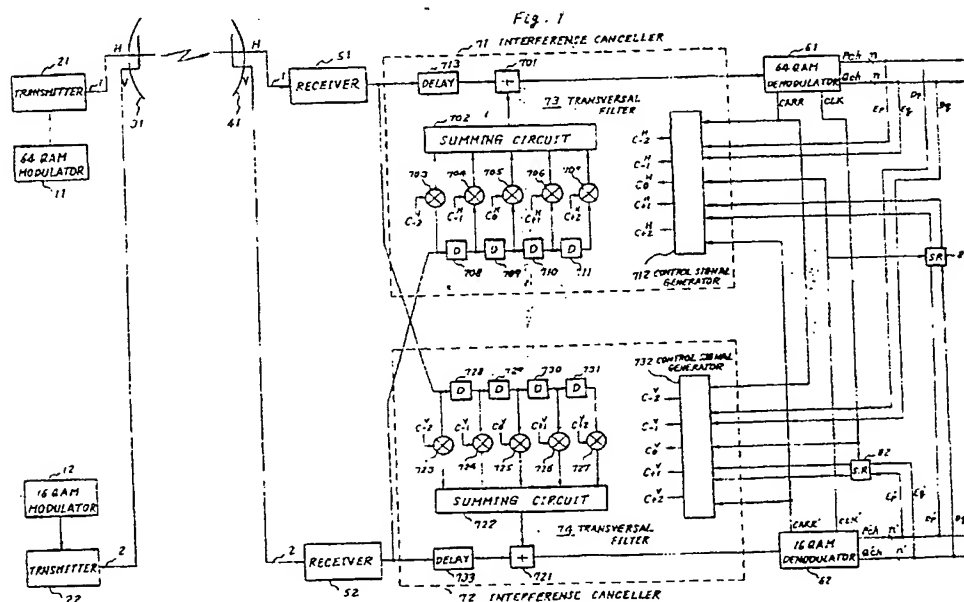
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Dual polarization transmission system.

A dual polarization transmission system for transmitting digital modulated signal each having a particular bandwidth by use of two polarized waves which have the same center frequency and are orthogonal to each other. The receiver side of the system demodulates radio frequency signals sent by a horizontally and a vertically polarized wave and coming in through a receiving antenna into IF signals. From the received signal of one polarization, an interference component of the other polarization generated on the basis of the cross-polar IF signal or demodulated signal is removed.



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DUAL POLARIZATION TRANSMISSION SYSTEM

The present invention relates to a dual polarization transmission system which transmits digital modulated signals having different bandwidths by radio waves that have the same center frequency and are different in polarization and, more particularly, to the cancellation of cross polarization interference components.

5 A transmission system of the type described uses a co-channel frequency arrangement in which two radio channels of horizontal polarization and vertical polarization share the same frequencies, and a particular bandwidth is assigned to each polarization. The co-channel frequency arrangement promotes effective use of frequencies without increasing the interface between co-polar channels, compared to an
10 interleaved frequency arrangement in which radio channels are alternately arranged on a horizontally and a vertically polarized wave. This type of transmission system is disclosed in U.S. Patent 4,861,021 issued to Yoshimoto and Maeda whose is one of the inventors of the present invention (Reference).

A system of the type transmitting signals having the same bandwidth by use of the co-channel frequency arrangement of radio channels of a horizontally (H-) and a vertically (V-) polarized wave is also known in the art. In relation to this type of system, there has been proposed an implementation for
15 cancelling cross polarization interference, i.e., the interface between a horizontally and a vertically polarized wave by Ryu, Tahara and Noguchi in the paper entitled "IF BAND CROSS POLARIZATION CANCELER" reported in ICC '84 LINKS FOR THE FUTURE, IEEE International Conference on Communication, held in Amsterdam, The Netherlands, May 14 - 17, 1984. (IEEE, 1984). It is not practicable, however, to apply the cross polarization interference cancellation (XPIC) for use with the co-channel frequency arrangement in
20 which a horizontally and a vertically polarized wave have the same bandwidth directly to the co-channel type transmission system which transmits signals having different bandwidths.

Specifically, an interference canceller for cancelling the interference between a H- and a V- polarized wave has a transversal filter therein. In the co-channel arrangement wherein the radio channels share the same bandwidth, the tap delay of the transversal filter is selected to be the reciprocal of the symbol rate f_s -
25 (equal to bandwidth) of signals to be transmitted. XPIC using such a transversal filter is not directly applicable to the dual polarization transmission system disclosed in Reference, since the latter assigns a different symbol rate to each of a H- and a V- polarized wave.

It is therefore an object of the present invention to provide a dual polarization transmission system capable of transmitting digital modulated signals having different bandwidths by different radio waves
30 having the same center frequency, while surely cancelling cross polarization interference components.

According to the invention, there is provided a dual polarization transmission system transmitting digital modulated signals having two different bandwidths by two orthogonal radio waves which have the same center frequency and are orthogonal in polarization, the system comprising, at a receiver side, interference
35 cancelling means for removing interference components leaked from a cross-polar wave from a co-polar received signal.

The above and other objects, features and advantages of the present invention will become more apparent from the following detailed description taken with the accompanying drawings in which:

- Fig. 1 is a block diagram schematically showing an embodiment of the dual polarization transmission system in accordance with the present invention;
- 40 Fig. 2 is a view representative of a frequency arrangement particular to the illustrative embodiment;
- Fig. 3 is a block diagram schematically showing a specific construction of a control signal generator included in the embodiment and having a phase error correcting circuit therein;
- Fig. 4 is a schematic block diagram showing a specific construction of the phase error correcting circuit;
- Fig. 5 and 6 are schematic block diagrams each showing a different alternative embodiment of the
45 present invention which, like the embodiment of Fig. 1, implements XPIC in the IF band; and
- Figs. 7 and 8 are schematic block diagrams each showing a different alternative embodiment of the present invention which implements XPIC in the baseband.

Referring to Fig. 1 of the drawings, a dual polarization transmission system embodying the present invention is shown. In Fig. 1, the transmitter side has a 64 QAM modulator 11, a 16 QAM modulator 12,
50 transmitters 21 and 22, and a transmitting antenna 31. The receiver side has receiving antenna 41, receivers 51 and 52, a 64 QAM demodulator 61, a 16 QAM demodulator 62, interference cancellers 71 and 72, and shift registers 81 and 82.

At the transmitter side, the 64 QAM modulator 11 produces a 64 QAM modulator signal (IF signal, center frequency f_{IF}) having a bandwidth B_1 ($=$ symbol rate f_{s1}). The transmitter 21 converts the 64 QAM modulated signal into a radio frequency signal whose center frequency is f_0 . This radio frequency signal is

applied to the horizontal polarization (H-polar) side of the transmitting antenna 31. On the other hand, the 16 QAM modulator 12 outputs a 16 QAM modulated signal (IF signal, center frequency f_{IF}) having a bandwidth

$$B_2 \quad (B_2 \approx B_1, B_2 = \text{symbol rate } f_{S2}).$$

5

The transmitter 22 associated with the modulator 12 converts the 16 QAM modulated signal into a radio frequency signal whose center frequency is f_0 , and the converted signal is applied to the vertical polarization (V-polar) side of the antenna 31. The antenna 31 radiates radio waves having been respectively
 10 polarized horizontally and vertically in the bandwidths B_1 and B_2 and at the center frequency f_0 . As a result, the arrangement of radio channels 1 and 2 is implemented, as shown in Fig. 2.

The symbol rate f_{S1} of the radio channels 1 is equal to the bandwidth B_1 . Assuming that the bit rate is α Mbit/s, then $f_{S1} = B_1 = \alpha/6$ MHz. The radio channels 2 also have a bit rate of α Mbit/s so that $f_{S2} = B_2 = \alpha/4$ MHz.

15 At the receiver side, the radio frequency signal coming in through the H-polar side of the antenna 41 and having the bandwidth B_1 is converted into an IF signal (center frequency f_{IF}) by the receiver 51. Likewise, the radio frequency signal coming in through the V-polar side of the antenna 41 is converted into an IF signal by the receiver 52. The IF signal from the receiver 51 is applied to the interference canceller 71 to cancel interference components from the cross-polarized wave, i.e. V-polarized wave. The output of the
 20 circuit 71 free from the interference components is led to the 64 QAM demodulator 61. In response, the demodulator 61 performs orthogonal detection. Then the demodulator 61 discriminates the orthogonal detected signal to produce as a baseband digital signal, a 3-bit regenerated data signal and a 1-bit error signal representative of a discrimination error in each of the P and Q channels as a baseband digital signal. In the same manner, the interference canceller 72 removes from the IF signal outputted by the receiver 52
 25 interference components from the cross-polarized wave, i.e. H-polarized wave. The 16 QAM modulator 62 effects orthogonal detection and then discrimination with the resulting output of the interference canceller 72, whereby a 2-bit regenerated data signal and a 1-bit error signal are produced from each of the P and Q channels as a baseband digital signal.

The interference canceller 71 is made up of a delay circuit 713, a transversal filter 73, a control signal
 30 generator 712, and an adder 701. The transversal filter 73 has delay circuits 708, 709, 710 and 722, 5-tap weighting circuits 703, 704, 705, 706 and 707, and a summing circuit, or summing circuit, 702. Adapted to set a tap delay, the delay circuits 708 to 711 are connected in series and each has the reciprocal $1/n \times B_2$ (n being an integer) of an integral multiple of the bandwidth assigned to the cross-polar side, i.e. V-polar side. The output of the receiver 52 is applied to the delay circuit 708. Applied to the weighting circuits 703 to 707
 35 are respectively the output of the receiver 52 and the outputs of the delay circuit 708 to 711. In response, the weighting circuits 703 to 707 delivers to the summing circuit 702 weighted signals each being proportional to respective one of control signals C_{-2}^H , C_{-1}^H , C_0^H , C_1^H , and C_2^H which are outputted by the control signal generator 712. The output of the transversal filter 73 is added by the adder 701 to the IF
 40 signal from the receiver 51 which is routed through a delay circuit 713 which compensates for the delay particular to the transversal filter 73. The output of the adder 701 which is free from the cross polarization interference component is applied to the 64 QAM demodulator 61. The delay of the delay circuit 713 is indispensable in compensating for the delay of the transversal filter 73 and thereby setting up the timing at the adder 701.

The control signal generator 712 receives an IF band carrier CARR (f_{IF} MHz) recovered by the 64 QAM
 45 demodulator 61, 1-bit error signals E_p and E_q representative of a discrimination error at the 64 QAM demodulator 61, an IF band carrier CARR' (f_{IF} MHz) recovered by the 16 QAM demodulator 62, a recovered clock signal CLK' (f_{S2}), and quadrant detection signals D'_p and D'_q which are, for example, the most significant bits (MSBs) of the regenerated data signals subjected to orthogonal detection by the carrier
 50 CARR'. At this instant, the quadrant detection signals D'_p and D'_q from the cross-polarized side, i.e., from the 16 QAM demodulator 62 has been delayed by the shift register 81 which operates at the timings of the recovered clock signal CLK' of the cross-polarized side, i.e., the 16 QAM demodulator 82. This is successful in compensating for the difference in delay time between the 64 QAM demodulator 62 and the 16 QAM demodulator 62 (i.e., difference in delay characteristic between roll-off filters built in the individual demodulators).

55 A reference will be made to Figs. 3 and 4 for describing a specific construction of the control signal generator 712. As shown in Fig. 3, the carrier CARR and the error signals E_p and E_q from the 64 QAM demodulator 61 and the carrier CARR' from the 16 QAM demodulator 82 are applied to a phase error correcting circuit 799. The phase error correcting circuit 799 corrects the difference in phase between the

quadrant detection signals D'_p and D'_q and the error signals E_p and E_q ascribable to the phase difference between the carriers $CARR$ and $CARR'$. More specifically, the signals propagated in orthogonal polarizations are reproduced by the carriers of the individual demodulators. Therefore, should a difference in phase exist between the individual carriers at the time of regeneration, the interference components from the orthogonal polarized sides and the signal components effected by the interference would be regenerated in different phases. The difference in phase has to be corrected. As shown in Fig. 4, the phase error correcting circuit 799 has a carrier phase comparator 781, inverters 782 and 783, and selectors 784 and 785. The carrier phase comparator 781 compares the phases of the carrier recovered by the 64 QAM and 16 QAM demodulators 61 and 62, respectively, and feeds control signals to the selectors 784 and 785 on the basis of the result of comparison. The error signals E_p and E_q from the 64 QAM demodulator 61 and inverted signals $\overline{E_p}$ and $\overline{E_q}$ from inverters 782 and 783 are applied respectively to the selectors 784 and 785. In response, the selectors 784 and 785 operate according to the control signals from the carrier comparator 781, as shown in Table below.

PHASE DIFFERENCE	0	$\pi/2$	π	$3/2\pi$
SELECTOR 782 OUTPUT	E_p	$\overline{E_q}$	$\overline{E_p}$	E_q
SELECTOR 783 OUTPUT	E_q	E_p	$\overline{E_q}$	$\overline{E_p}$

In the above Table, $\overline{E_p}$ and $\overline{E_q}$ are representative of the opposite phases of E_p and E_q , respectively.

Referring again to Fig. 3, the control signal generator 712 is made up of flip-flops 786 to 781 operated by the clock signal which is recovered by the 16 QAM demodulator 62, and correlation detectors 792 to 796 each having an integrator therein. The flip-flops 788 to 791 are connected in series. The error signals E_p and E_q are fed to one input of the correlation detectors 792 to 796 via the flip-flops 786 and 787, while the branched output signals of the phase error correcting circuit 799 and the outputs of the flip-flops 788 to 791 are applied to the other input. The correlation detectors 792 to 796 produce respectively weighting control signals C_{-2} , C_{-1} , C_0 , C_{+1} and C_{+2} each being representative of a correlation between the error signal of the co-polar side and the quadrant detection signal of the cross-polar side. More specifically, by determining the correlation between the error signals of the co-polar side and the quadrant detection signals of the cross-polar side, the correlation detectors 792 to 796 estimate interference components from the cross-polar side remaining in the output of the adder 701. By such estimation, the tap coefficient is controlled to cause the transversal filter 73 to generate interference components, thereby minimizing the remaining interference components.

In the illustrative embodiment, the phase error correcting circuit 799 is connected to the input side where the error signals of the co-planar side arrive. Alternatively, the phase error correcting circuit 799 may be connected to the input side where the quadrant detection signals D'_p and D'_q from the 16 QAM demodulator 62 arrive. In such a case, the difference in phase between the quadrant detection signals and the error signals ascribable to the difference in phase between the carriers recovered by the individual demodulators will be corrected.

In Fig. 1, the interference canceller 72, like the interference canceller 71, has a delay circuit 733, a transversal filter 74, an adder 721, and a control signal generator 732. The interference canceller 72 differs from the interference canceller 71 regarding the delay of the delay circuit 733, the delays of delay circuit 728 to 731 built in the transversal filter 74, and the input to the control signal generator 732. Specifically, the delay circuit 733 has a delay which compensates for the delay particular to the transversal filter 74, while the delay circuits 728 to 731 each has a delay of $1/m\omega B_1$ (m being an integer) which is the reciprocal of an integral multiple of the bandwidth of the cross-polar side, i.e. H-polar side. The control signal generator 732 receives the recovered carrier $CARR$, recovered clock signal CLK (f_{s1}) and quadrant detection signals D_p and D_q from the 64 QAM demodulator 61, and the recovered carrier $CARR'$ and error signals E'_p and E'_q from the 16 QAM demodulator 62. At this instant, the error signals E'_p and E'_q from the demodulator 62 are delayed by a shift register 82 which is operated at the timings of the recovered clock signal CLK from the 64 QAM demodulator 61, so that the difference in delay time between the 64 QAM and 16 QAM demodulators 61 and 62 may be compensated for. The rest of the construction and operation is identical with the horizontal polarization side, and redundant description will be avoided for simplicity.

In the illustrative embodiment, the quadrant detection signals D'_p and D'_q and error signals E'_a and E'_q from the 16 QAM demodulator 62 are delayed by the shift registers 81 and 82, on the assumption that the

internal delay time of the 64 QAM demodulator 61 is longer than that of the 16 QAM demodulator 62. Alternatively, the output of either one of the demodulators having a shorter delay time than the other may be delayed by taking account of the internal delay time of each demodulator.

In Fig. 5, an alternative embodiment of the present invention shown. The following description will concentrate only on the portions of the alternative embodiment which are different from the previous embodiment. As shown, the alternative embodiment has an interference canceller 71' which is constituted by a transversal filter 75 for generating interference components from the cross-polarized side, an adder 701 for adding the output of the transversal filter 75 and the output of a delay circuit 741 to produce a signal free from interference components, a control signal generator 746 for delivering weighting control signals to the transversal filter 75, and a delay circuit 741 for delaying the IF signal from the receiver 51 by the same delay time as the transversal filter 75. Delay circuits 742, 743, 744 and 745 arranged in the transversal filter 75 each has a delay of $1/n' \times B_1$ (n' being an integer greater than or equal to 2) which is the reciprocal of the bandwidth of the co-polar side, i.e. the H-polarized side.

Why the transversal filter 75 can produce a desired corrected signal despite the delay of $1/n' \times B_1$ is as follows. A H- wave and a V- wave (or interference wave in this case) are respectively limited to $f_{s1}/2$ and $f_{s2}/2$ in the baseband. The signal to be generated by a transversal filter of an interference canceller is an approximate signal of an interference wave. According to the sampling theorem, an interference wave limited in band to the maximum frequency $f_{s2}/2$ can be fully representative by the values sampled by frequencies higher than f_{s2} . Hence, desired corrected signals are achievable only if the tap delays of the transversal filters incorporated in the individual interference cancellers are less than $1/f_{s2}$ of the interference wave. It follows that the delay of $1/n' \times B_1$ of the delay circuits 742 and 745 which is smaller than $1/f_{s2}$ is desirable. However, the delay of $1/B_1$ is acceptable if a little performance degradation is allowed.

The illustrative embodiment further includes demodulators 91 and 92 adapted for cross-polarized waves. Specifically, the demodulator 91 receives the output of the delay circuit 743 incorporated in the transversal filter 75, i.e., the V-polarized IF signal. The demodulator 91 demodulates the output of the delay circuit 743 by using the recovered carrier CARR and recovered clock signal CLK from the demodulator on the H-polar side, i.e., the 64 QAM demodulator 61, thereby producing quadrant detection signals $D'p$ and $D'q$. The control signal generator 746 outputs weighting control signals in response to the recovered clock signal CLK and error signals E_p and E_q from the demodulator at the co-polar side, i.e., the 64 QAM demodulator 61 and the quadrant detection signals $D'p$ and $D'q$ from the demodulator 91. At this instant, the demodulator 91 demodulates the inputs by the recovered carrier CARR from the 64 QAM demodulator 61, so that the control signal generator 746 shown in Fig. 3 does not need a phase error correcting circuit. To correct the delay time difference between the two demodulators, it is necessary that either the error signals E_p and E_q from the demodulator 61 or the quadrant detection signals $D'p$ and $D'q$ from the demodulator 91 be delayed at the timings of the recovered clock signal CLK. In this particular embodiment, the quadrant detection signals $D'p$ and $D'q$ are delayed by the shift register 81, on the assumption that the internal delay of the demodulator 91 is small.

The interference canceller 72' located at the V-polarized side is similar in construction to the interference canceller 71' stated above. Specifically, the interference canceller 72' has a transversal filter 76 made up of delay circuits 752 to 755 each having a delay of $1/m \times B_2$ (m being an integer) which is the reciprocal of an integral multiple of the bandwidth of the co-polar side, i.e., the V-polar side, weighting circuits 723 to 727, and a summing circuit 722. A delay circuit 751 delays the IF signal from the receiver 52 by a delay of the transversal filter 76. An adder 721 adds the output of the delay circuit 751 and the output of the transversal filter 76 to produce a signal free from interference components. The reference numeral 756 designates a control signal generator. The demodulator 92 demodulates and regenerates the output of the delay circuit 753 (H-polarized IF signal) by the recovered carrier CARR' and recovered clock signal CLK' from the 16 QAM demodulator 62 of the cross-polar side, thereby producing quadrant detection signals D_p and D_q .

The control signal generator 756 outputs weighting control signals C_{-2}^V , C_{-1}^V , C_0^V , C_{+1}^V and C_{+2}^V in response to the recovered clock signal CLK' and error signals $E'p$ and $E'q$ from the 16 QAM demodulator 62 and the quadrant detection signals D_p and D_q from the demodulator 92. The error signals $E'p$ and $E'q$ and quadrant detection signals D_p and D_q are applied to input terminals 798 and 797 of the control signal generator, in Fig. 3, and from which the phase correcting circuit is omitted. The shift register 82 delays the error signals $E'p$ and $E'q$ at the timings of the recovered clock signal CLK'.

This embodiment differs from the embodiment of Fig. 1 in that the tap delay of the transversal filter of the interference canceller located on the co-polar side is the reciprocal of an integral multiple of the bandwidth of the co-polar side, and in that the clock signal of co-polar side is fed to the control signal generator. In such a configuration, the outputs of the individual receivers suffice the interface between the

H- and V-polarization systems. Hence, when the demodulator on one of the opposite sides fails, the interface canceller associated with the different polarization is normally operable. Furthermore, in the case that each system is accommodated in an independent housing, a single connecting portion suffices.

Fig. 6 shows another alternative embodiment of the present invention which is essentially similar to the embodiment of Fig. 5 except that delay circuits 762 to 765 and 772 to 775 incorporated in transversal filters 77 and 78, respectively, have delays each being the reciprocal of an integral multiple of the bandwidth of the H-polarized wave. Specifically, in Fig. 6, the delays of the delay circuits 762 to 765 and 772 to 775 each is the reciprocal $1/n' \times B_1$ (n' being an integer) of an integral multiple of the bandwidth of the H-polar side. The recovered clock signal CLK from the 64 QAM modulator 61 is applied to the demodulator 92, control signal generator 776, and shift register 82. The delay circuit 771 has the same delay time as that of the transversal filter 77. Regarding the rest of the construction and operation, this embodiment is identical with the embodiment of Fig. 5.

The illustrative embodiment assigns a delay which is the reciprocal of an integral multiple of the bandwidth of the H-polar side to the delay circuits built in the two transversal filters, as stated above. Hence, the interference cancellers each being associated with particular polarization can be implemented with an identical construction.

While the embodiment of Fig. 6 has been shown and described as adopting the reciprocal of an integral multiple of the bandwidth of the horizontal polarization as the tap delay of both of the transversal filters, it may be replaced with the reciprocal of an integral multiple of the bandwidth of the vertical polarization. Then, the recovered clock of the V-polar side will be applied to the each of the control signal generators.

All the embodiments described so far cancel cross polarization interference in the IF band. The interference may alternatively be cancelled in the baseband, as will be described.

In Fig. 7, another alternative embodiment of the present invention is shown which cancels interference components ascribable to cross-polarization waves before the discrimination of data, i.e., in analog signals and in the baseband. Fig. 7 shows only the receiving side. A radio frequency signal coming in through the antenna 41 and having the bandwidth B_1 of the H-polar side is converted into an IF signal by the receiver 51 and then applied to the 64 QAM demodulator 61 and the demodulator 92 adapted for the cross-polar side. A radio frequency signal coming in through the antenna 41 and having the bandwidth B_2 of the V-polar side is converted into an IF signal by the receiver 52 and then applied to the 16 QAM demodulator 62 and the demodulator 91 adapted for the cross-polar side. The demodulators 61, 62, 91 and 92 are made up of orthogonal synchronous detectors 611, 621, 911 and 912 and discriminators 612, 622, 912 and 922, respectively.

The IF signals from the receivers 51 and 52 are respectively demodulated by orthogonal synchronous detectors 611 and 621 into P channel and Q channel signals of the baseband. At the same time, and IF signals from the receivers 51 and 52 are respectively applied to orthogonal synchronous detectors 921 and 911 to be thereby converted into P channel and Q channel signals of the baseband by the recovered carriers CARR and CARR' adapted to 64 QAM and 16 QAM. The output signals of the orthogonal synchronous detectors 611 and 621 are respectively routed through interference cancellers 79 and 80 to the discriminators 612 and 622 and thereby converted into baseband digital signals. The output signals of the orthogonal synchronous detectors 911 and 912 are also routed through the interference cancellers 79 and 80 to the discriminators 912 and 922, respectively. In response, the discriminators 912 and 922 convert their inputs into digital signals by discriminating them by the 64 QAM recovered clock signal CLK and the 16 QAM recovered clock signal CLK', respectively.

The interference canceller 79 has transversal filters 954 and 955 to which the P channel and Q channel outputs of the orthogonal synchronous detector 911 respectively are applied. Adders 942 and 942' receive the outputs of the transversal filters 954 and 955, respectively. Delay circuits 930 and 930' delay respectively the P channel and Q channel outputs of the detector 611. An adder 931 adds the output of a delay circuit 930 and the output of the adder 942, while an adder 931' adds the output of a delay circuit 930' and the output of the adder 942'. The resulting outputs of the adders 931 and 931' are fed to a discriminator 612. The reference numeral 953 designates a control signal generator.

Delay circuits 932 to 935 and delay circuits 943 to 946 incorporate in the transversal filters 954 and 955, respectively, each are connected in series and have a delay which is the reciprocal $1/n \times B_1$ (n being an integer) of an integral multiple of the bandwidth of the horizontal polarization. The P channel and Q channel outputs of the orthogonal synchronous detector 911 are connected to the delay circuits 932 and 943, respectively. The output of the detector 911 and the outputs of the delay circuits 932, 933, 943 and 935 are fed to weighting circuits 936, 937, 938, 939 and 940, respectively. The weighting circuits 936 to 940 each delivers to a summing circuit 941 a weighted signal which is proportional to a control signal fed from the control signal generator 953. At the same time, the output of the detector 911 and the outputs of the delay

circuits 932, 933, 934 and 935 are delivered to weighting circuits 936', 937', 938', 939' and 940', respectively. In response, the weighting circuits 936' to 940' each feeds to a summing circuit 941' a weighted signal which is proportional to control signal fed from the control signal generator 953.

Further, the output of the detector 911 and the outputs of the delay circuits 943 to 946 are fed to weighting circuits 947 to 951 and 947' to 951'. In response, the weighting circuits 947 to 951 and 947' to 951' deliver to summing circuits 952 and 952', respectively, weighted signals which are proportional to control signals fed from the control signal generator 953. As a result, an interference component from the P channel of the 16 QAM modulated signal to the P channel of the 64 QAM modulated signal, an interference component from the P channel of the 16 QAM modulated signal to the Q channel of the 64 QAM modulated signal, an interference component from the Q channel of the 16 QAM modulated signal to the P channel of the 64 QAM modulated signal, and an interference component from the Q channel of the 16 QAM modulated signal to the Q channel of the 64 QAM modulated signal appear on the output terminals of the summing circuits 941, 941', 952 and 952', respectively.

More specifically, the correlations between the error signals of the co-planar side and the quadrant detection signals of the cross-polar side are detected to estimate interference components from the cross-polar side to the P channel of the co-polar side remaining in the output of the adder 931. By such estimation, the tap coefficient is controlled to cause the transversal filter to generate interference components such that the remaining interference components are minimized. Likewise, the transversal filter is caused to generate interference components such that the interference components from the cross-polar side to the Q channel of the co-polar side remaining in the output of the adder 931'.

An adder 942 adds the outputs of the summing circuits 941 and 952, i.e., the interference components to the P channel of the 64 QAM modulated signal, while an adder 942' adds the outputs of the summing circuits 941' and 952', i.e., the interference components to the Q channel of the 64 QAM modulated signal.

Adders 931 and 931' add respectively the P channel and Q channel outputs of the orthogonal synchronous detectors 611 routed through the delay circuits 930 and 930' and the outputs of the adders 942 and 942'. The outputs of the adders 931 and 931' which are free from interference components are applied to the discriminator 612.

The delay circuits 930 and 930' compensate for the difference in delay time between the route extending from the receiver 51 to the adders 931 and 931' via the orthogonal synchronous detector 611 and the route extending from the receiver 52 to the adders 931 and 931' via the orthogonal synchronous detector 911 and transversal filters 954 and 955.

Signals appearing on the center taps of the transversal filters 934 and 955 are applied to the discriminator 912. In response, the discriminator 912 outputs quadrant detection signals D_p and D_q in synchronism with the recovered clock fed thereto from the discriminator 612.

The quadrant detection signals D_p and D_q from the discriminator 912 are delivered to the control signal generator 953 together with the recovered clock signal CLK and, error signals E_p and E_q among the baseband digital signal from the discriminator 612. Based on these signals, the control signal generator 953 produces weighting control signals by the previously stated method.

An interference canceller 80 is constructed in the same manner as the interference canceller 79 except for the differences which will be described. Specifically, delay circuits 957 to 960 and 968 to 971 incorporated in the interference canceller 80 each has a delay which is the reciprocal $1/m \times B_2$ (m being an integer) of an integral multiple of the bandwidth assigned to the V-polar side. Delay circuits 956 and 956' compensate for the difference in delay time between the route extending from the receiver 52 to the adders 981 and 981' via the orthogonal synchronous detector 621 and the route extending from the receiver 51 to the adders 981 and 981' via the orthogonal synchronous detector 921 and transversal filters 979 and 980.

Fig. 8 shows another alternative embodiment of the present invention which executes digital processing in the baseband. In Fig. 8, like in Fig. 7, only the receiver side is shown. A radio frequency signal coming in through the antenna 41 and having the bandwidth B_1 assigned to the H-polar side is converted into an IF signal by the receiver 51 and then fed to the 64 QAM demodulator 61 and the demodulator 92 adapted for the cross-polar side. A radio frequency signal also coming in through the antenna 41 and having the bandwidth B_2 assigned to the V-polar side is converted into an IF signal by the receiver 52 and then applied to the 16 QAM demodulator 62 and the demodulator 91 adapted for the cross-polar side.

The P channel and Q channel baseband digital signals demodulated and regenerated by the 64 QAM demodulator 61 are applied respectively to delay circuits 101 and 101' which are included in an interference canceller 79. The input to the demodulator 91 is demodulated and regenerated in response to the recovered carrier CARR and recovered clock signal CLK from the 64 QAM demodulator 61 and then fed to transversal filters 125 and 126.

Delay circuits 103 to 106 and 114 to 117 included in the transversal filters 125 and 126, respectively,

each has a delay which is the reciprocal $1/nxB_1$ (n being an integer) of an integral multiple of the bandwidth assigned to the H-polar side.

The P channel baseband digital signal from the demodulator 91 and the outputs of the delay circuits 103, 104, 105 and 106 are applied respectively to the weighting circuits 107 to 111 and 107' to 111'. The weighting circuits 107 to 111 and 107' to 111' each produces a weighted signal proportional to a weighting control signal and feeds it to associated one of summing circuits 112 and 112'. Likewise, the Q channel baseband digital signal from the demodulator 91 and the outputs of the delay circuits 114 to 117 are fed respectively to weighting circuits 118 to 122 and 118' to 122'. The weighting circuits 118 to 122 and 118' to 122' each produces a weighted signal proportional to a weighting control signal and delivers it to associated one of summing circuits 123 and 123'.

An adder 102 adds the P channel baseband digital signal from the 64 QAM demodulator 61 routed through the delay circuit 101 and the output of an adder 113 which is the sum of the summing circuits 112 and 123. Likewise, an adder 102' adds the Q channel baseband digital signal from the 64 QAM demodulator 61 routed through the delay circuit 101' and the output of an adder 113' which is the sum of the summing circuits 112' and 123'. The adders 102 and 102', therefore, produce signals which are free from interference components.

A control signal generator 124 receives the recovered clock signal CLK from the 64 QAM demodulator 61, error signals E_p and E_q included in the outputs of the adders 102 and 102', and quadrant detection signals D_p and D_q included in the outputs of the center taps of the transversal filters 125 and 126. In response, the control signal generator 124 produces control signals meant for the weighting circuits 107 to 111, 107' to 111', 118 to 122, and 118' to 122'.

An interference canceller 80', like the interference canceller 79', removes from the output of the 16 QAM demodulator 62 the interference components from the cross-polar side which are produced from the output of the demodulator 92. Delay circuits 129 to 132 and 140 to 143 included in transversal filters 151 to 152, respectively, each has a delay which is the reciprocal $1/mxB_2$ (m being an integer) of an integral multiple of the bandwidth assigned to the V-polar side.

In the illustrative embodiments of Figs. 7 and 8 which cancel cross polarization interference in the baseband, it is assumed that the transversal filters included in the interference cancellers each has a tap interval equal to the reciprocal of an integral multiple of the bandwidth of the co-polar side. In practice, however, three different tap intervals are available as previously stated in relation to the interference cancellation in the IF band, i.e., the reciprocal of the bandwidth assigned to the co-polar side, the reciprocal of the bandwidth assigned to the cross-polar side, and either one of them.

It is to be noted that the present invention is practicable with any suitable multi-level QAM modulated signals other than the 64 QAM and 16 QAM modulated signals shown and described. It is also to be noted that the present invention is practicable with phase shift keying (PSK) modulated signals.

In summary, in a dual polarization transmission system of the type transmitting digital modulated signals having different bandwidths by radio waves which have the same center frequency and are different in polarization, the present invention has interference cancellers capable of cancelling interference components introduced from the cross-polar side into the received signal of the co-polar side. The present invention, therefore, frees demodulated signals from degradation in quality.

Either one of the error signals of the co-polar side applied to a control signal generator included in each interference canceller and quadrant detection signals of the cross-polar side is delayed by a shift register. This is successful in compensating for a difference in internal delay between demodulators assigned to opposite polarization sides.

The embodiment shown in Fig. 1 is practicable with a simple construction partly because delay circuits incorporated in transversal filters assigned to opposite polarization sides each has a delay which is the reciprocal of an integral multiple of the bandwidth of the cross-polar side and partly because use is not made of a demodulator adapted for the cross-polar side.

In the embodiment of Fig. 5, each transversal filter assigned to a particular polarization side has delay circuits whose delay is the reciprocal of an integral multiple of the bandwidth of the co-polar side, and a demodulator for the cross-polar side is associated with each of the opposite polarization sides. This allows a 64 QAM and a 16 QAM system to be interfaced at a single point of each receiver. Hence, even when one demodulator fails, it does not affect the interference canceller of the cross-polar side.

Further, the embodiment shown in Fig. 6 implements interference cancellers of opposite polarization sides with an identical configuration since delay circuits built in transversal filters each has a delay which is the reciprocal of an integral multiple of the bandwidth of one polarization side.

Claims

1. A dual polarization transmission system for transmitting each of digital modulated signals having two different bandwidths by respective one of radio waves which have a same center frequency and are orthogonal in polarization to each other, said system comprising at a receiver side;
 5 cross polarization interference cancelling means for removing a cross-polar interference component from a co-polar received signal.
2. A system as claimed in claim 1, wherein said cross polarization interference cancelling means comprises:
 10 a transversal filter having a predetermined tap delay for producing cross-polarization interference components;
 control signal generating means for feeding a weighting control signal to said transversal filter; and
 adding means for adding an output of said transversal filter to the co-polar digital modulated signal to cancel said cross-polarization interference components.
3. A system as claimed in claim 2, wherein said predetermined tap delay of said transversal filter
 15 corresponds to a reciprocal of an integral multiple of the bandwidth assigned to a cross-polarized wave.
4. A system as claimed in claim 2, wherein said predetermined tap delay of said transversal filter corresponds to a reciprocal of an integral multiple of the bandwidth assigned to a co-polarized wave.
5. A system as claimed in claim 2, wherein said predetermined tap delay of said transversal filter corresponds to a reciprocal of an integral multiple of the bandwidth assigned to either one of polarized
 20 waves having a narrower bandwidth than the other.
6. A system as claimed in any of claims 2 to 5, wherein said control signal generating means receives an error signal representative of discrimination error for a co-polar regenerated data signal, and a regenerated data signal and a recovered clock signal derived from a cross-polar transmitted signal.
7. A system as claimed in any of claims 2 to 5, wherein said control signal generating means receives an
 25 error signal representative of discrimination error for a co-polar regenerated data signal and a recovered clock signal of co-polar side, and a regenerated data signal derived from a cross-polar transmitted signal.
8. A system as claimed in claim 6 or 7, further comprising delaying means for delaying either one of the error signal representative of discrimination error for the co-polar regenerated data signal and the regenerated data signal derived from the cross-polar transmitted signal to produce a delayed signal, and for
 30 delivering said delayed signal to said control signal generating means.
9. A dual polarization transmission system for transmitting each of digital modulated signals having two different bandwidths by respective one of radio waves which have a same center frequency and are orthogonal in polarization to each other, said system comprising a transmitter side and a receiver side;
 35 said transmitter side comprising:
 a first and a second modulator each for outputting respective one of digital modulated signals having the two different bandwidths;
 a first and a second transmitter each for converting respective one of outputs of said first and second modulators into a radio frequency signal having a same center frequency; and
 a transmitting antenna for radiating output signals of said first and second transmitters as radio waves which
 40 are orthogonal in polarization to each other;
 said receiver side comprising:
 a receiving antenna for receiving the radio waves on a polarization basis and thereby producing a first and a second radio frequency signal, respectively;
 a first and a second receiver for converging said first and second radio frequency signals into a first and a
 45 second IF signal, respectively;
 first and second cross polarization interference cancelling means for removing interference components of orthogonal polarization from outputs of said first and second receivers on the basis of said first and second IF signals, respectively; and
 a first and a second demodulator for demodulating respectively outputs of said first and second cross polarization interference cancelling means to discriminate and regenerate said outputs.
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10. A system as claimed in claim 9, wherein said first and second cross polarization interference cancelling means each comprises:
 a transversal filter having a predetermined tap delay for receiving a cross-polar digital modulated signal to generate a cross-polar interference component;
 55 control signal generating means for feeding a weighting control signal to said transversal filter;
 adding means for adding an output of said transversal filter to a co-polar digital modulated signal to feed a signal free from cross polarization interference components to said demodulator.
11. A system as claimed in claim 10, wherein said transversal filters of said first and second cross

polarization interference cancelling means each has a predetermined tap delay which is a reciprocal of an integral multiple of the bandwidth assigned to the cross-polarized wave;

said control signal generating means each generating and weighting control signal in response to an error signal from said first demodulator and a recovered clock signal and a regenerated data signal from said second demodulator.

12. A system as claimed in claim 10 or 11, further comprising delaying means for delaying either one of said co-polar error signal and said cross-polar regenerated data signal and for delivering said delayed signal to said control signal generating means.

13. A dual polarization transmission system for transmitting each of digital modulated signals having two different bandwidths by respective one of radio waves which have a same center frequency and are orthogonal in polarization to each other, said system comprising at a receiver side:

first receiving means for converting a radio frequency signal transmitted by co-polar one of the two orthogonal polarized waves into an IF signal;

second receiving means for converting a radio frequency signal transmitted by cross-polar one of the two orthogonal polarized wave into an IF signal;

first detecting means for detecting a co-polar error signal by demodulating the IF signal outputted by said first receiving means;

second detecting means for detecting a cross-polar regenerated data signal by demodulating the IF signal outputted by said second receiving means;

control signal generating means for generating a weighting control signal from said co-polar error signal and said cross-polar regenerated data signal;

a transversal filter applied with said IF signal of cross-polar side and having a tap delay which is weighted in proportion to said weighting control signal to generate cross-polar interference component; and

adding means for removing the cross-polar interference component from said co-polar IF signal to deliver an output thereof to said first detecting means.

14. A system as claimed in claim 13, wherein the tap delay of said transversal filter has a delay which is a reciprocal of an integral multiple of the bandwidth assigned to the cross-polarized wave;

said control signal generating means for generating said weighting control signal in synchronism with a clock which is produced by said second detecting means.

15. A system as claimed in claim 13, wherein the tap delay of said transversal filter has a delay which is a reciprocal of an integral multiple of the bandwidth assigned to the co-polarized wave;

said control signal generated means generating said weighting control signal in synchronism with a clock produced by said first detecting means.

16. A system as claimed in claim 13, wherein a predetermined intertap delay time of said transversal filter has a delay which is synchronous to a reciprocal of either one of the bandwidths assigned to the co-polarized and cross-polarized waves;

said control signal generating means generating said weighting control signal in synchronism with either one of clock signals produced by said first and second detecting means.

17. A system as claimed in any of claims 13 to 16, further comprising delaying means for delaying either one of said co-polar error signal and said cross-polar regenerated data signal to be applied to said control signal generating means, and delivering said delayed signal to said control signal generating means.

18. A dual polarization transmission system for transmitting digital modulated signals each having respective one of a first and a second bandwidth by a first and a second polarized waves which have a same center frequency and orthogonal in frequency to each other, said system comprising at a receiver side:

first receiving means for converting the radio frequency signal having the first bandwidth and transmitted by the first polarized wave into a first IF signal;

second receiving means for converting the ratio frequency signal having the second bandwidth and transmitted by the second polarized wave into a second IF signal;

first detecting means for demodulating said first IF signal to produce a first demodulated signal and detecting an error signal out of a signal from which cross polarization interference has been removed;

adding means for producing said signal from which cross polarization interference has been removed from said demodulated signal and interference components;

second detecting means for demodulating said second IF signal to produce a second demodulated signal and detecting a regenerated data signal out of said second demodulated signal;

control signal generating means for generating a weighting control signal from said error signal and said regenerated data signal; and

a transversal filter for receiving said second demodulated signal and having a predetermined tap delay weighted in proportion to said weighting control signal to generate said interference component.

19. A system as claimed in claim 18, wherein said predetermined tap delay has a delay which is a reciprocal of an integral multiple of the bandwidth assigned to the second polarized wave.

20. A system as claimed in claim 18, wherein said predetermined tap delay has a delay which is a reciprocal of an integral multiple of the bandwidth assigned to the first polarized wave.

5 21. A system as claimed in any of claims 18 to 20, further comprising delay means for delaying either one of said error signal and said regenerated data signal and feeding said delayed signal to said control signal generating means.

22. A dual polarization transmission system for transmitting digital modulated signals each having respective one of a first and a second bandwidth by a first and a second polarized wave which have a same
10 center frequency and orthogonal in frequency to each other, said system comprising at a receiver side; first receiving means for converting the radio frequency signal having the first bandwidth and transmitted by the first polarized wave into a first IF signal;

second receiving means for converting the radio frequency signal having the second bandwidth and transmitted by the second polarized wave into a second IF signal;

15 first detecting means for demodulating and regenerating said first IF signal to produce a baseband digital signal including a first regenerated data signal and a first error signal;

second detecting means for demodulating and regenerating said second IF signal to produce a baseband signal including a second regenerated data signal and a second error signal;

20 first control signal generating means for generating a first weighting control signal from said first error signal and said second regenerated data signal;

a first transversal filter for receiving said second baseband digital signal and having a first tap delay weighted in proportion to said first weighting control signal to generate a first interference component;

second control signal generating means for generating a second weighting control signal from said second error signal and said first regenerated data signal;

25 a second transversal filter for receiving said first baseband digital signal and having a second predetermined tap delay weighted in proportion to said second weighting control signal to generate a second interference component;

first adding means for removing said first interference component from said first baseband digital signal; and

30 second adding means for removing said second interference component from said second baseband digital signal.

23. A system as claimed in claim 22, wherein said first and second predetermined tap delays have delays which are respectively reciprocals of integral multiples of the bandwidths assigned to the second and first polarized waves.

35 24. A system as claimed in claim 22, wherein said first and second predetermined tap delays have delays which are respectively reciprocals of integral multiples of the bandwidths assigned to the first and second polarized waves.

25. A system as claimed in claim 22, wherein said first and second predetermined tap delays have delays which are synchronous to a reciprocal of the bandwidth assigned to either one of the first and second
40 polarized waves.

26. A system as claimed in claim 22, further comprising a first and a second delaying means for delaying respectively either one of said first error signal and said first quadrant detection signal and either one of said second quadrant detection signal and said second error signal and feeding said delayed signals to said first and second control signal generating means.

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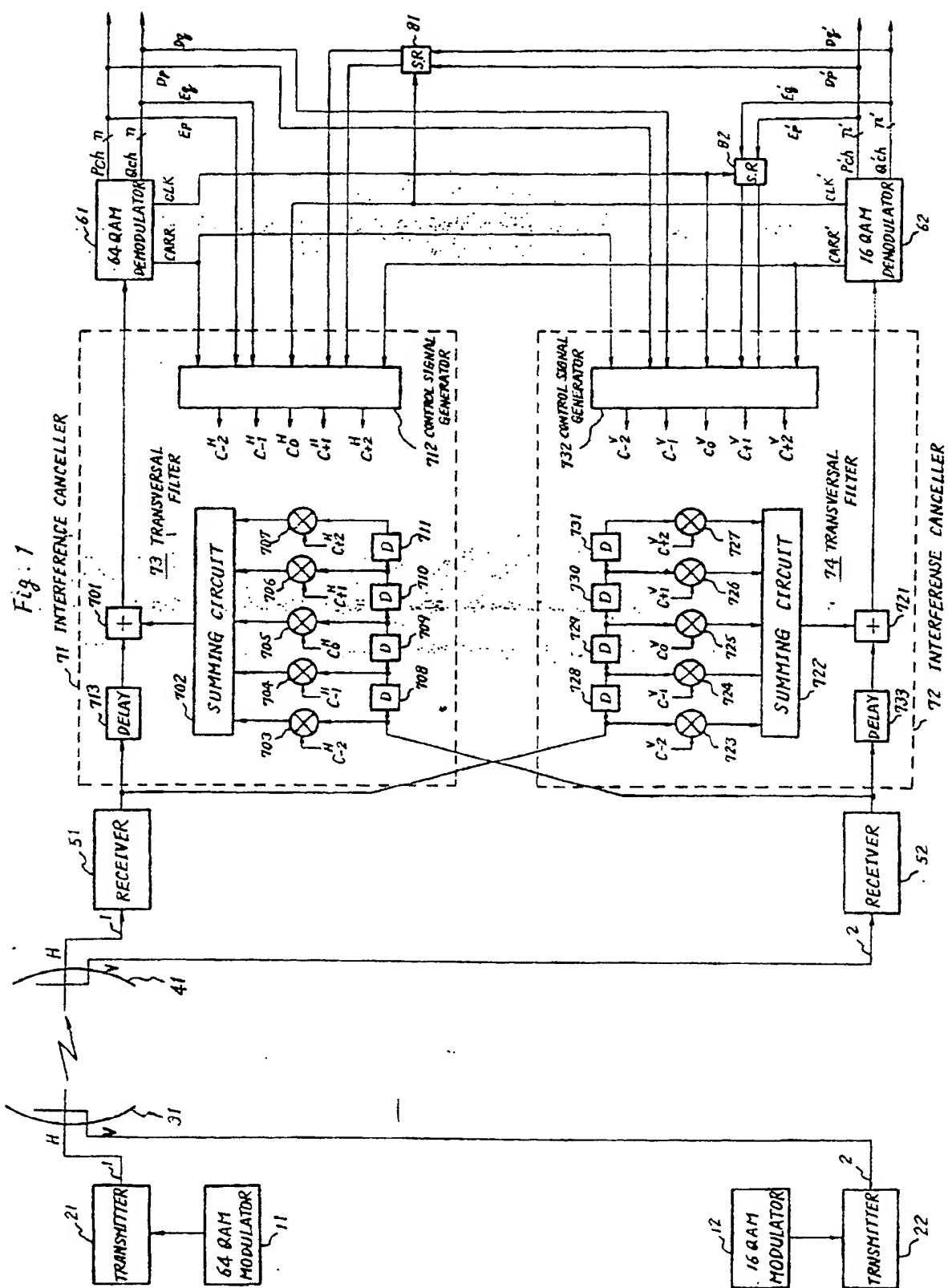


Fig. 2

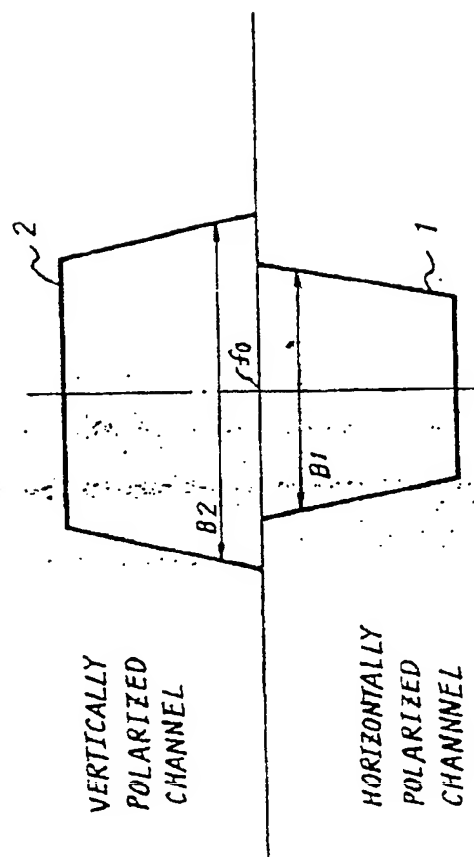
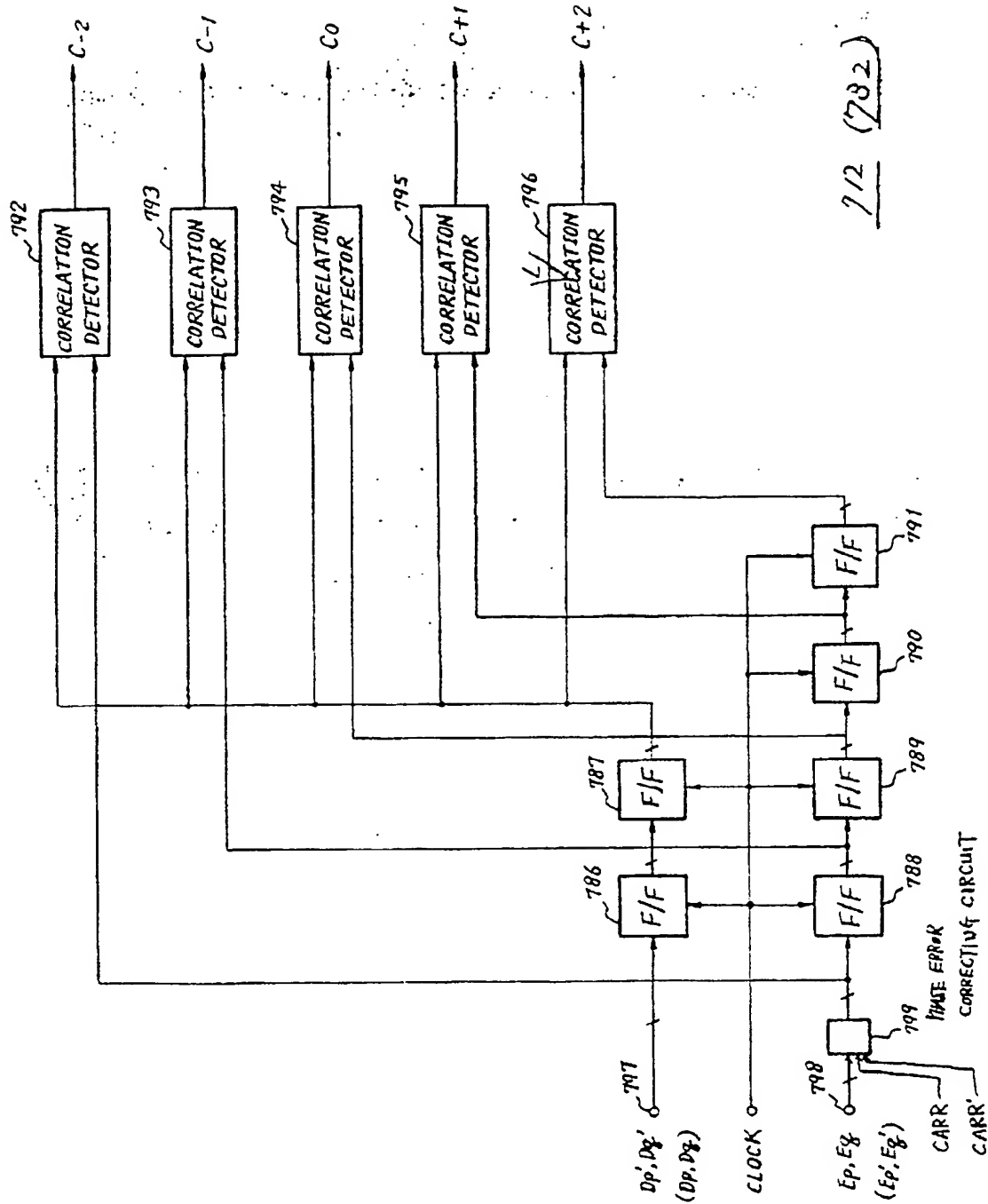


Fig. 3



712 (732)

Fig. 4

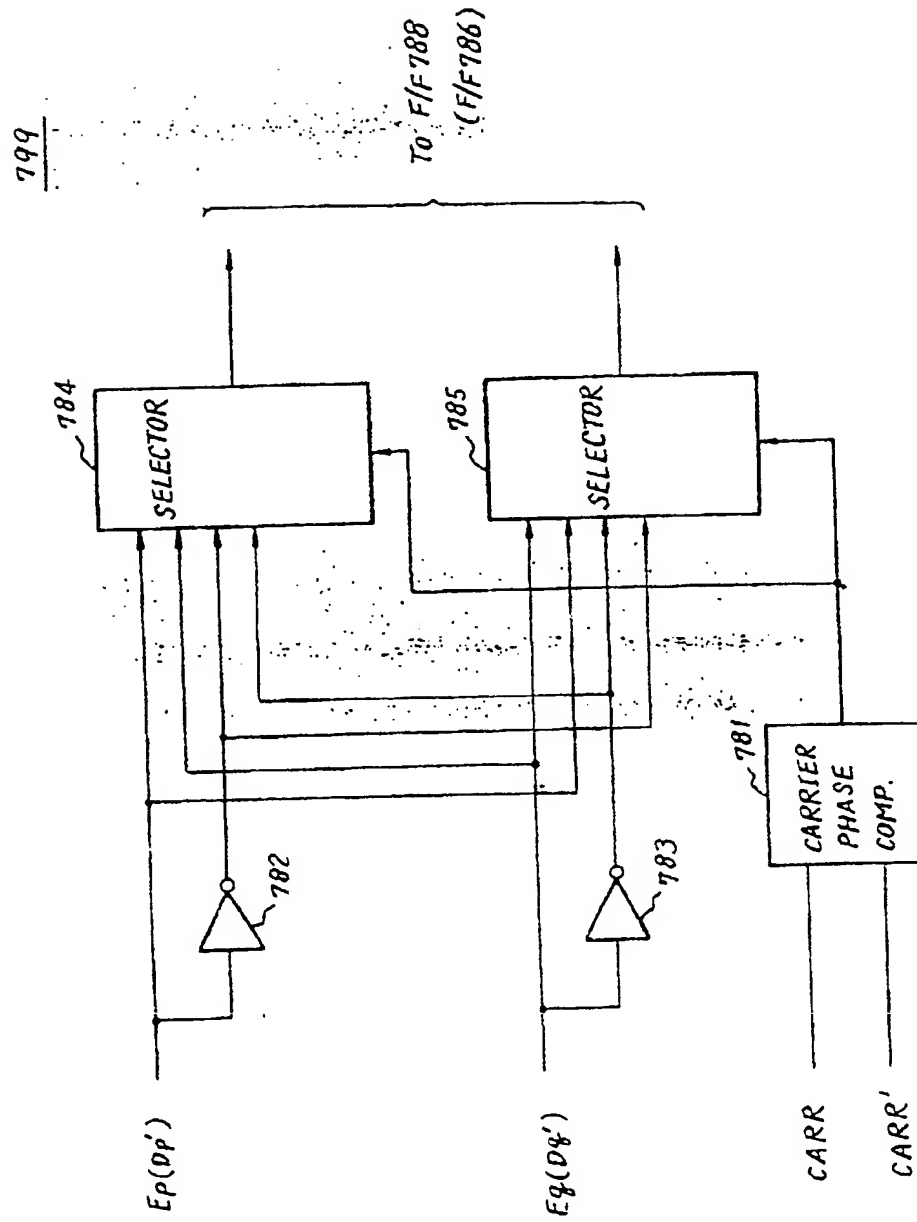


Fig. 5

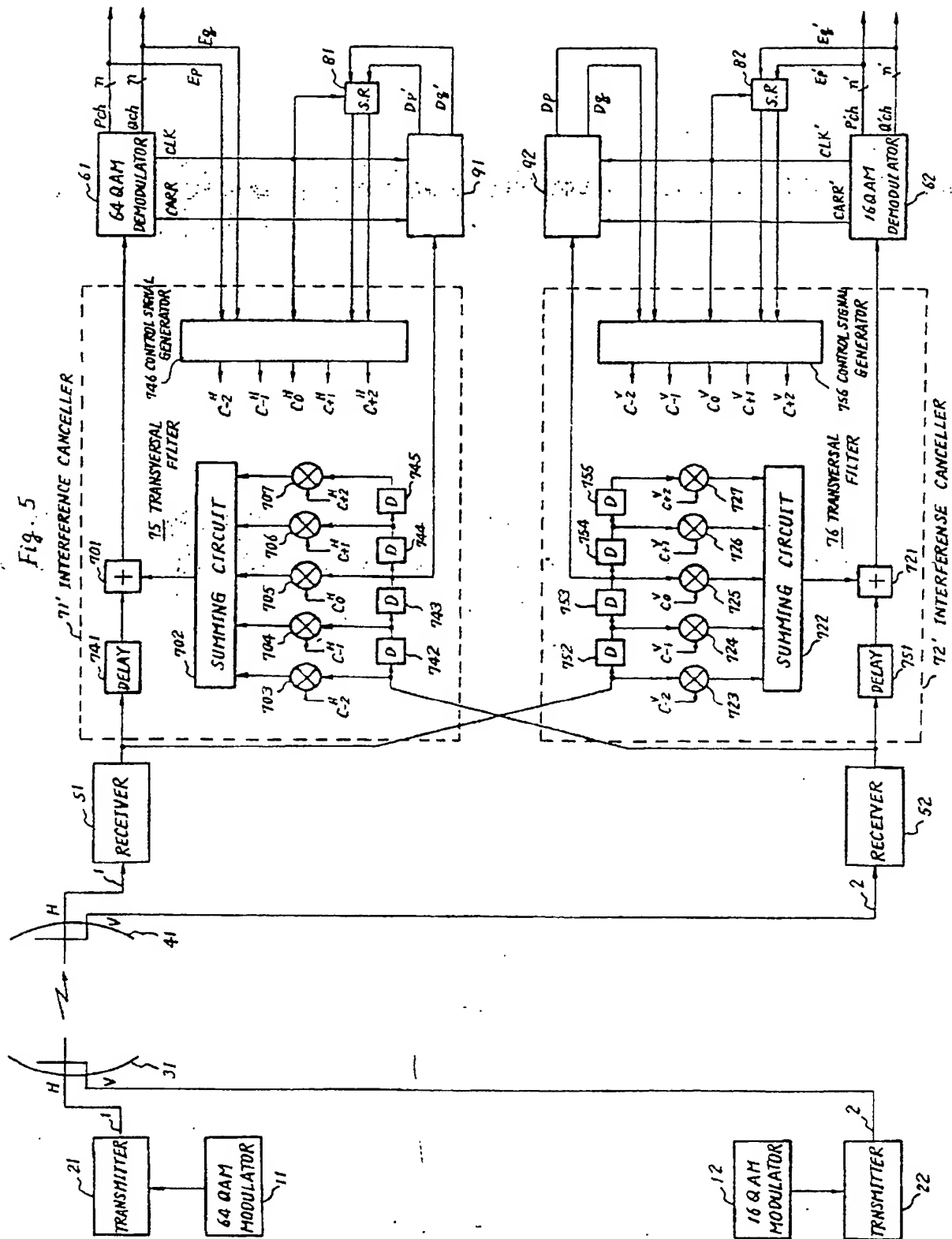


Fig. 6

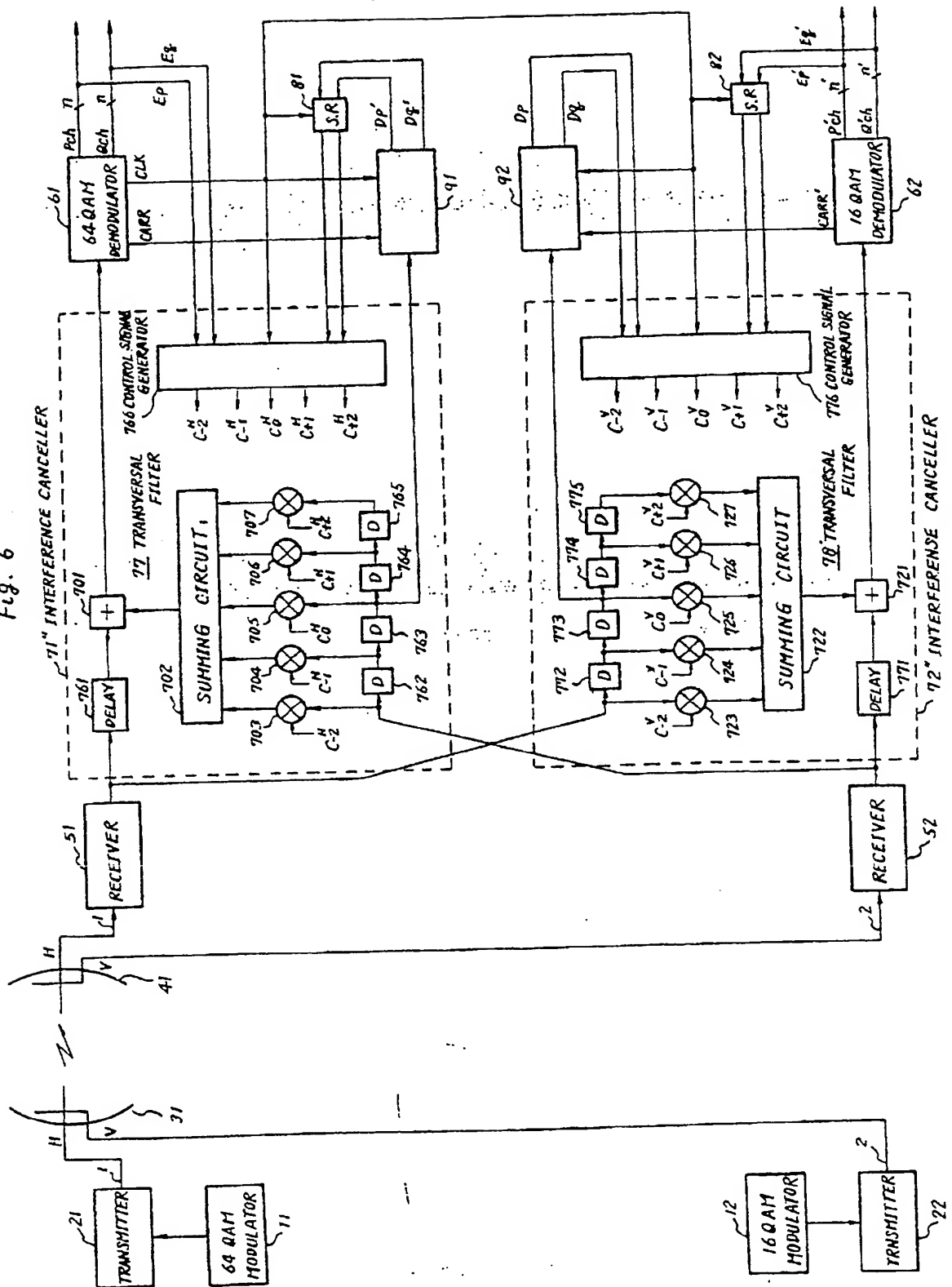


Fig. 7

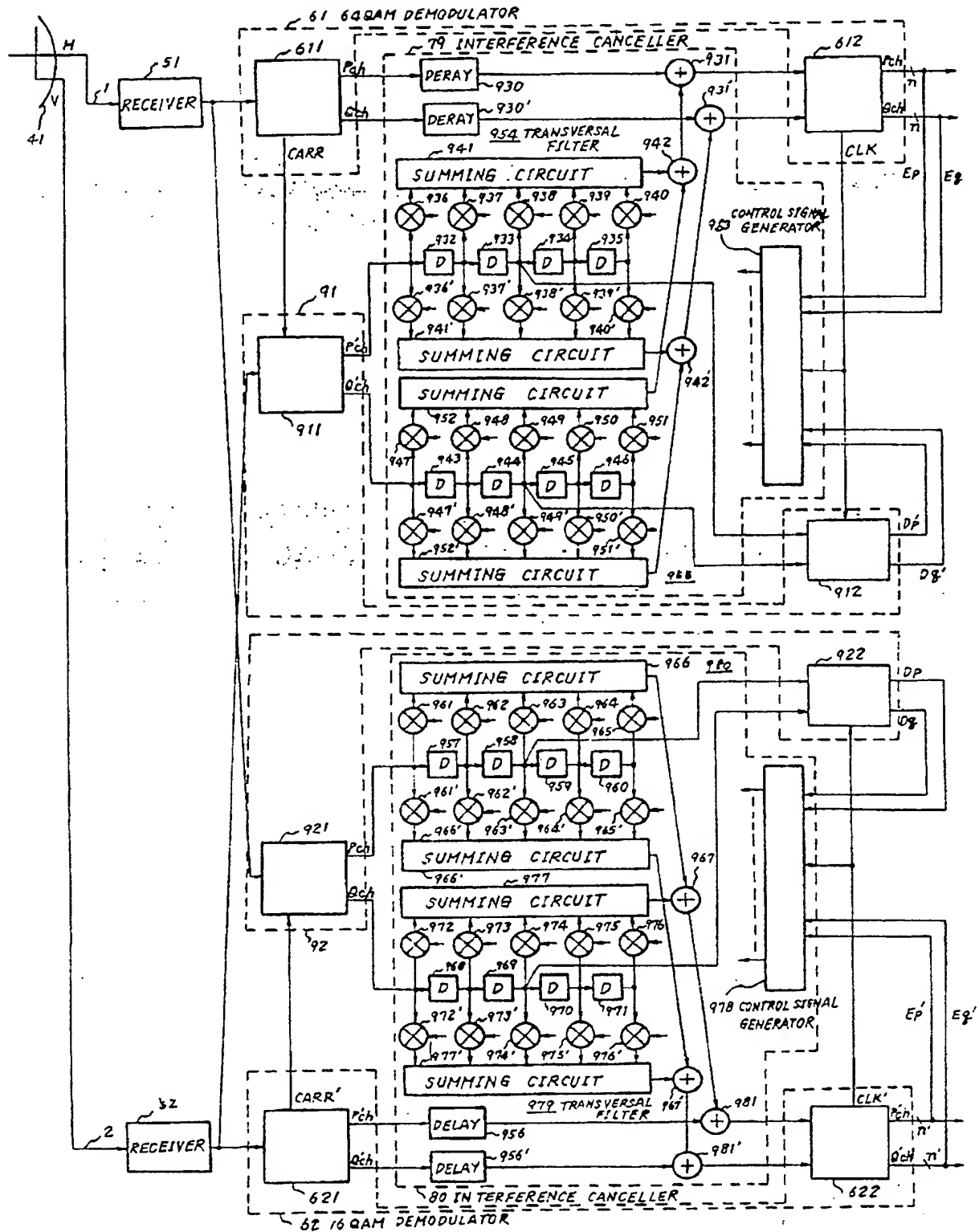
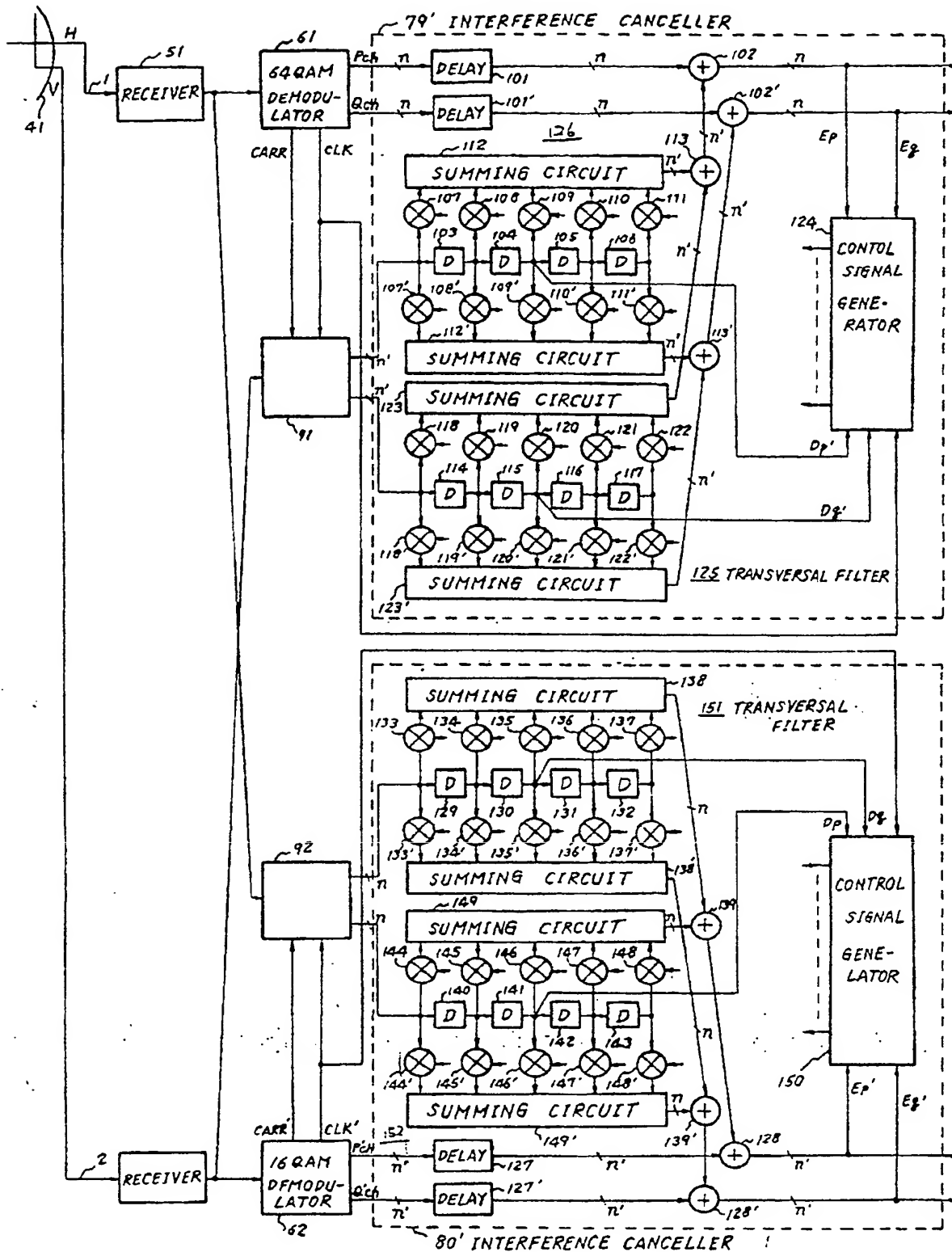


Fig. 8



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Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 418 781 A3

(12)

EUROPEAN PATENT APPLICATION

(21) Application number: 90117858.2

(51) Int. Cl.⁵: **H04B 7/00**

(22) Date of filing: 17.09.90

(30) Priority: 18.09.89 JP 242892/89
16.05.90 JP 126162/90
17.05.90 JP 128059/90

(43) Date of publication of application:
27.03.91 Bulletin 91/13

(84) Designated Contracting States:
DE FR GB IT

(58) Date of deferred publication of the search report:
27.11.91 Bulletin 91/48

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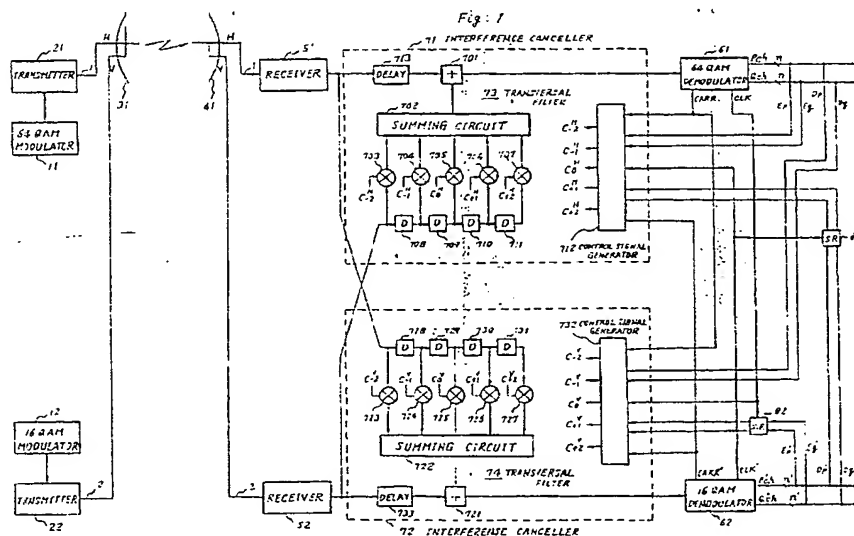
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(54) **Dual polarization transmission system.**

(57) A dual polarization transmission system for transmitting digital modulated signal each having a particular bandwidth by use of two polarized waves which have the same center frequency and are orthogonal to each other. The receiver side of the system demodulates radio frequency signals sent by

a horizontally and a vertically polarized wave and coming in through a receiving antenna into IF signals. From the received signal of one polarization, an interference component of the other polarization generated on the basis of the cross-polar IF signal or demodulated signal is removed.

**EP 0 418 781 A3**



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Patent Office

EUROPEAN SEARCH REPORT

Application Number

EP 90 11 7858

DOCUMENTS CONSIDERED TO BE RELEVANT					
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)		
Y	EP-A-0 295 620 (NEC CORP.) * Column 3, lines 41-55; column 5, lines 17-34; figure 6 * & US-A-4 861 021 (Cat. D)	1,2,9,18	H 04 B 7/00		
A	---	13,22			
Y	SIEMENS TELCOM REPORT, vol. 11, no. 1, January/February 1988, pages 22-25; B. LANKL et al.: "Gleichkanalbetrieb auch bei extremer Depolarisation" * Page 23, column 1, line 25 - page 23, column 3, line 14; figures 1,2 *	1,2,18			
A	IDEM	6,7,10,22			
D,Y	PROCEEDINGS OF THE ICC'84, Amsterdam, 14th - 17th May 1984, vol. 3, pages 1442-1446; T. RYU et al.: "IF band cross polarization canceler" * Page 1444; figure 6 *	9			
A	IDEM	6,7,10,13			
A	EP-A-0 244 779 (SIEMENS AG) * Abstract; figure 1 *	3-5,11, 14-16,19, 20,23-29	TECHNICAL FIELDS SEARCHED (Int. Cl.5) H 04 B H 04 L		
The present search report has been drawn up for all claims					
Place of search The Hague		Date of completion of search 19 September 91	Examiner BOSSEN M.		
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